

## 5. Energy Equation

**1. Ideal fluid (理想流體) :** Ideal fluid is a fluid assumed to be "inviscid" (non-viscous fluid) 非黏性流體

Mathematically :  $\mu = 0$

→ 為何要假設為理想流體？

Ans : 假設為理想流體即表示流體粒子間，或流體與邊界間無黏滯力作用，故所有加諸在流體上之力，均用以產生加速度，無需克服阻力。

**2. Distinctions between various fluids and flows (各種流體與流況之區別) :**

① Newtonian fluid  $\left( \tau_{yx} = \mu \frac{du}{dy} \right)$

Non-Newtonian fluid

② Incompressible fluid ( $\rho = \text{const.}$ )

Compressible fluid

③ Steady flow  $\left( \frac{\partial(\quad)}{\partial t} = 0 \right)$

Unsteady flow

④ Irrotational flow ( $\vec{\Omega} = 0$ )

Rotational flow

⑤ Ideal fluid (Inviscid fluid, Non-viscous fluid) ( $\mu = 0$ )

Real fluid (Viscid fluid, Viscous fluid)

⑥ Laminar flow (層流)

Turbulent flow (亂流)

**3. 1-D Euler's Eqn. (along the streamline)**

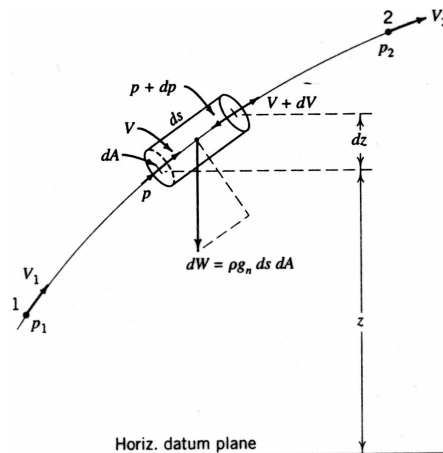


Fig. 5.1

因為是 Inviscid fluid ( $\mu = 0$ ) → No viscous force (無需考慮黏滯剪應力  $\tau$ )

→ 所受到的力：① Pressure, ② Gravity

① Pressure force:

$$P \cdot dA - (P + dP)dA = -dP \cdot dA$$

② Gravity force:

$$dW = \rho g \cdot dA \cdot ds$$

$$\text{Streamline dir. : } -dW \cdot \sin \theta = -\rho g \cdot dA \cdot ds \cdot \frac{dz}{ds}$$

$$= -\rho g \cdot dA \cdot dz$$

③  $F_s = m \cdot a_s$

$$F_s = (-dP \cdot dA - \rho g \cdot dA \cdot dz)$$

$$m = \rho \cdot dA \cdot ds$$

$$a_s = V \cdot \frac{dV}{ds} \quad (\text{Recall Chap.3})$$

$$-dP \cdot dA - \rho g \cdot dA \cdot dz = (\rho \cdot dA \cdot ds) \left( V \cdot \frac{dV}{ds} \right)$$

$$-dP - \rho g \cdot dz = \rho V \cdot dV$$

$$\rightarrow \frac{dP}{\rho} + g \cdot dz + V \cdot dV = 0$$

$$\text{or } \boxed{\frac{dP}{\rho g} + dz + \frac{dV^2}{2g} = 0} \quad \text{1-D Euler's eqn. (along the streamline)}$$

For Incompressible fluid: ( $\rho = \text{const.}$ )

$$d \left( \frac{P}{\rho g} + z + \frac{V^2}{2g} \right) = 0$$

#### 4. Bernoulli's Eqn. along the Streamline

Integrating 1-D Euler's eqn. (along the streamline)

$$\boxed{\frac{P}{\gamma} + z + \frac{V^2}{2g} = \text{constant} = H} \quad \text{Bernoulli's eqn. (along the streamline)}$$

◎ Assumptions (適用條件): ①  $\mu = 0$  (Inviscid fluid) 理想流體

②  $\rho = \text{const.}$  (Incompressible fluid)

③ Along the streamline (1-D)

④ steady flow

Bernoulli's eqn. is a useful relationship between  $P$ ,  $V$ , and  $z$ .

where  $H \equiv$  Total head (總水頭)

$\frac{P}{\gamma} \equiv$  pressure head (壓力水頭)

$z \equiv$  elevation head (高度水頭)

$\frac{V^2}{2g} \equiv$  velocity head (速度水頭)

### 5. Energy line (EL) and Hydraulic Grade line (HGL)

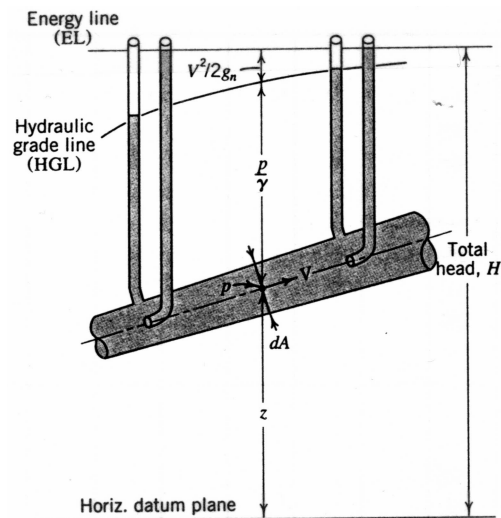


Fig. 5.2

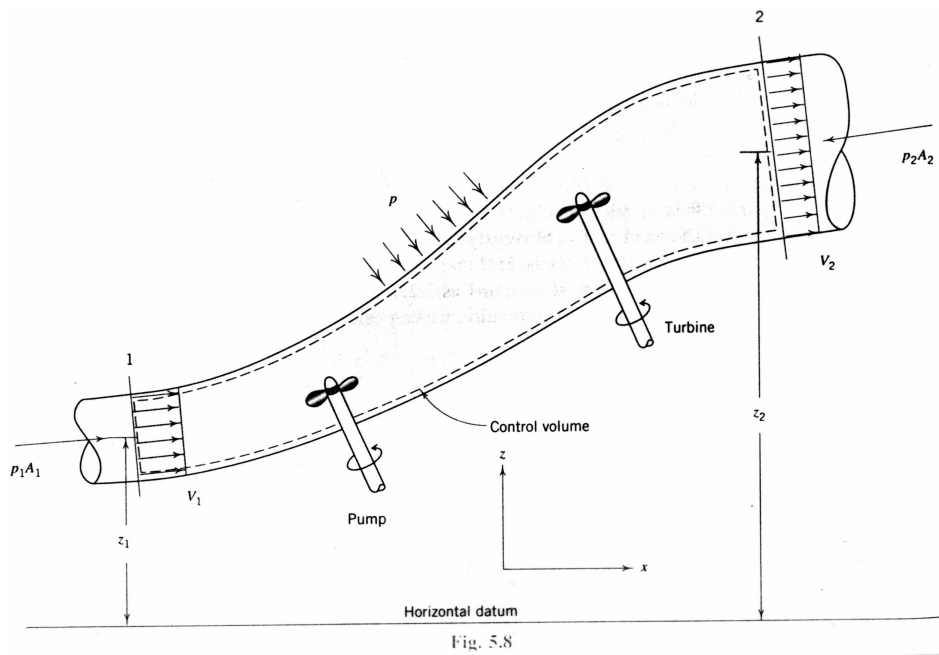
① Energy line (EL)  $\equiv$  Total head line (可用 Stagnation Tube 量測)

$$\left( \frac{P}{\gamma} + z + \frac{V^2}{2g} \right) \text{ 總和之連線}$$

② Hydraulic grade line (HGL)  $\equiv$  Piezometric head line (可用 Piezometer 量測)

$$\left( \frac{P}{\gamma} + z \right) \text{ 總和之連線} \quad (\text{稱為 piezometric head or hydraulic head})$$

## 6. Work-Energy Equation



### ● Mechanical work-energy principle:

(Heat transfer and internal energy are neglected.)

$$dW = dE$$

where  $dW$  = the work done on a fluid system

$dE$  = the change in P.E. and K.E. of a fluid system

$$\rightarrow \frac{dW}{dt} = \frac{dE}{dt}$$

① For steady flow and incompressible fluid:

$$\frac{dE}{dt} = \iint_{c.s.} \rho \vec{V} \cdot d\vec{A}$$

$$\text{where } e = \frac{E}{m} = \frac{\frac{1}{2}mV^2 + mgz}{m} = \frac{V^2}{2} + gz$$

$$\begin{aligned} \frac{dE}{dt} &= \iint_{c.s.} \rho \left( \frac{V^2}{2} + gz \right) \vec{V} \cdot d\vec{A} \\ &= \rho \left( \frac{V_2^2}{2} + gz_2 \right) V_2 A_2 - \rho \left( \frac{V_1^2}{2} + gz_1 \right) V_1 A_1 \\ &= Q\gamma \left[ \left( \frac{V_2^2}{2g} + z_2 \right) - \left( \frac{V_1^2}{2g} + z_1 \right) \right] \end{aligned}$$

②  $\frac{dW}{dt}$  : Two parts

(1) Surface forces: <i> Normal: pressure (✓)

<ii> Shear: friction (✗)

$$\begin{aligned}\frac{dW}{dt} &= \oint_{c.s.} (-pd\vec{A}) \cdot \vec{V} \quad (\text{Power} = \vec{F} \cdot \vec{V}) \\ &= P_1 A_1 V_1 - P_2 A_2 V_2 \\ &= Q(P_1 - P_2)\end{aligned}$$

(2) Mechine work: Turbine  $\frac{dW}{dt} = -Q\gamma E_T$

$$\text{Pump} \quad \frac{dW}{dt} = +Q\gamma E_P$$

Where  $E_T$  = energy extracted by turbine per unit weight of fluid

$E_P$  = energy added by pump per unit weight of fluid

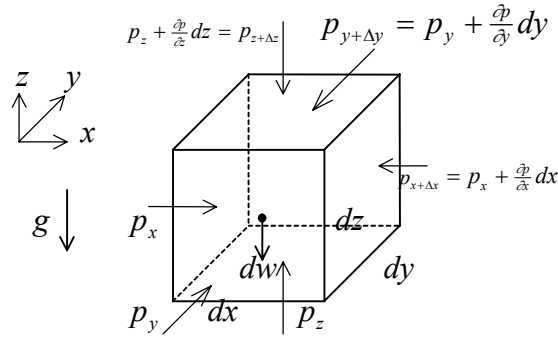
$$\begin{aligned}\Rightarrow \frac{dW}{dt} &= \frac{dE}{dt} \\ &= Q(P_1 - P_2) + (Q\gamma E_P - Q\gamma E_T) \\ &= Q\gamma \left( \frac{P_1}{\gamma} - \frac{P_2}{\gamma} \right) + Q\gamma (E_P - E_T) \\ &= Q\gamma \left( \frac{P_1}{\gamma} - \frac{P_2}{\gamma} + E_P - E_T \right) \\ &= Q\gamma \left[ \left( \frac{V_2^2}{2g} + z_2 \right) - \left( \frac{V_1^2}{2g} + z_1 \right) \right]\end{aligned}$$

$$\therefore \boxed{\frac{P_1}{\gamma} + z_1 + \frac{V_1^2}{2g} + E_P = \frac{P_2}{\gamma} + z_2 + \frac{V_2^2}{2g} + E_T} \quad \text{Work-Energy Equation}$$

$$\text{Power:} \quad \frac{Q\gamma (E_T \text{ or } E_P) \frac{ft \cdot lb}{s}}{550} = hp \quad (\text{U.S. units})$$

$$\frac{Q\gamma (E_T \text{ or } E_P) \frac{J}{s}}{1000} = kW \quad (\text{SI units})$$

### 7. 3-D Euler's Equation



Without viscosity (No shear)

→ Only Pressure (normal stress) and gravity (body force)

$$\textcircled{1} \sum F_x = P_x d y d z - \left( P_x + \frac{\partial P}{\partial x} d x \right) d y d z = - \frac{\partial P}{\partial x} d x d y d z$$

$$\textcircled{2} \sum F_y = P_y d x d z - \left( P_y + \frac{\partial P}{\partial y} d y \right) d x d z = - \frac{\partial P}{\partial y} d x d y d z$$

$$\textcircled{3} \sum F_z = P_z d x d y - \left( P_z + \frac{\partial P}{\partial z} d z \right) d x d y - \rho d x d y d z \cdot g = - \frac{\partial P}{\partial z} d x d y d z - \rho g d x d y d z$$

We know :

$$a_x = u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} + \frac{\partial u}{\partial t} = \frac{D u}{D t}$$

$$a_y = u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} + \frac{\partial v}{\partial t} = \frac{D v}{D t}$$

$$a_z = u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} + \frac{\partial w}{\partial t} = \frac{D w}{D t}$$

$$\vec{F} = m \vec{a} = (\rho d x d y d z) \vec{a}$$

$$\textcircled{1} F_x = m a_x = (\rho d x d y d z) a_x = - \frac{\partial P}{\partial x} d x d y d z$$

$$\therefore \rho a_x = \rho \left[ u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} + \frac{\partial u}{\partial t} \right] = - \frac{\partial P}{\partial x}$$

$$\textcircled{2} F_y = m a_y = (\rho d x d y d z) a_y = - \frac{\partial P}{\partial y} d x d y d z$$

$$\therefore \rho a_y = \rho \left[ u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} + \frac{\partial v}{\partial t} \right] = - \frac{\partial P}{\partial y}$$

$$\textcircled{3} F_z = ma_z = (\rho dx dy dz) a_z = -\frac{\partial P}{\partial z} dx dy dz - \rho g dx dy dz$$

$$\therefore \rho a_z = -\frac{\partial P}{\partial z} - \rho g = \rho \left[ u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} + \frac{\partial w}{\partial t} \right]$$

整理如下：

$$\rho a_x = \rho \frac{Du}{Dt} = -\frac{\partial P}{\partial x} + \rho g_x$$

$$\rho a_y = \rho \frac{Dv}{Dt} = -\frac{\partial P}{\partial y} + \rho g_y$$

$$\rho a_z = \rho \frac{Dw}{Dt} = -\frac{\partial P}{\partial z} + \rho g_z = -\frac{\partial P}{\partial z} - \rho g$$

如令  $\vec{g} = g_x \hat{i} + g_y \hat{j} + g_z \hat{k}$  則  $g_x = g_y = 0, g_z = -g$

故 Euler's Eqn. 通式  $\boxed{\rho \frac{D\vec{V}}{Dt} = -\nabla P + \rho \vec{g}}$  Eqn. of Motion (or Momentum eqn.)  
for ideal and incompressible fluid

$\Rightarrow$  can solve 4 unknowns :  $u, v, w, P$   
by 3 eqns. of motion ( $x, y, z$  方向)  
and 1 continuity eqn.  $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$

## 8. Bernoulli's Eqn. in flowfield

Integrating Euler's eqn. for incompressible fluid and steady flow

$$\times dx \quad \textcircled{1} -\frac{1}{\rho} \frac{\partial p}{\partial x} = u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z}$$

$$\times dy \quad \textcircled{2} -\frac{1}{\rho} \frac{\partial p}{\partial y} = u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z}$$

$$\times dz \quad \textcircled{3} -\frac{1}{\rho} \frac{\partial p}{\partial z} - g = u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z}$$

---


$$\begin{aligned} \sum \Rightarrow -\frac{1}{\rho} \left( \frac{\partial p}{\partial x} dx + \frac{\partial p}{\partial y} dy + \frac{\partial p}{\partial z} dz \right) &= \left( u \frac{\partial u}{\partial x} dx + v \frac{\partial u}{\partial y} dx + w \frac{\partial u}{\partial z} dx \right) \\ &+ \left( u \frac{\partial v}{\partial x} dy + v \frac{\partial v}{\partial y} dy + w \frac{\partial v}{\partial z} dy \right) \\ &+ \left( u \frac{\partial w}{\partial x} dz + v \frac{\partial w}{\partial y} dz + w \frac{\partial w}{\partial z} dz \right) + g dz \end{aligned}$$

$$\begin{aligned}
\Rightarrow -\frac{1}{\rho}(dP) &= \left[ \frac{\partial\left(\frac{u^2}{2}\right)}{\partial x} dx + \frac{\partial\left(\frac{v^2}{2}\right)}{\partial x} dx + \frac{\partial\left(\frac{w^2}{2}\right)}{\partial x} dx \right] \\
&+ \left[ \frac{\partial\left(\frac{u^2}{2}\right)}{\partial y} dy + \frac{\partial\left(\frac{v^2}{2}\right)}{\partial y} dy + \frac{\partial\left(\frac{w^2}{2}\right)}{\partial y} dy \right] \\
&+ \left[ \frac{\partial\left(\frac{u^2}{2}\right)}{\partial z} dz + \frac{\partial\left(\frac{v^2}{2}\right)}{\partial z} dz + \frac{\partial\left(\frac{w^2}{2}\right)}{\partial z} dz \right] \\
&\left[ -v \frac{\partial v}{\partial x} dx - w \frac{\partial w}{\partial x} dx - u \frac{\partial u}{\partial y} dy - w \frac{\partial w}{\partial y} dy - u \frac{\partial u}{\partial z} dz - v \frac{\partial v}{\partial z} dz \right] \\
&+ \left( v \frac{\partial u}{\partial y} dx + u \frac{\partial v}{\partial x} dy \right) + \left( w \frac{\partial u}{\partial z} dx + u \frac{\partial w}{\partial x} dz \right) + \left( w \frac{\partial v}{\partial z} dy + v \frac{\partial w}{\partial y} dz \right) + g dz \\
&= d\left(\frac{u^2}{2} + \frac{v^2}{2} + \frac{w^2}{2}\right) + \left[ \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}\right)(ud y - vd x) \right] + \left[ \left(\frac{\partial w}{\partial y} - \frac{\partial v}{\partial z}\right)(vd z - wd y) \right] \\
&+ \left[ \left(\frac{\partial u}{\partial z} - \frac{\partial w}{\partial x}\right)(wd x - ud z) \right] + g dz \\
\left(\times \frac{1}{g}\right) \Rightarrow -\frac{dP}{\gamma} &= \frac{d(u^2 + v^2 + w^2)}{2g} + \frac{1}{g} \left[ \Omega_x(vd z - wd y) + \Omega_y(wd x - ud z) + \Omega_z(ud y - vd x) \right] + dz
\end{aligned}$$

$\Rightarrow$  Integration :

$$\boxed{\frac{P}{\gamma} + \frac{V^2}{2g} + z = H - \frac{1}{g} \int \left[ \Omega_x(vd z - wd y) + \Omega_y(wd x - ud z) + \Omega_z(ud y - vd x) \right]}$$

● Bernoulli's eqn. (any two points in flowfield) valid for ①  $\mu = 0$  (Euler's eqn.)

②  $\rho = \text{const}$

③ steady flow

④ irrotational ( $\vec{\Omega} = 0$ )



- If rotational, only valid when  $(v dz - w dy) = (w dx - u dz) = (u dy - v dx) = 0$

$$\Rightarrow \frac{dx}{u} = \frac{dy}{v} = \frac{dz}{w} \quad (\text{streamline function})$$

$\Rightarrow$  Bernoulli's eqn. only valid along streamline in rotational flows.

## 5. Energy Equation for Ideal Fluid

1. Ideal fluid (理想流體) : Ideal fluid is a fluid assumed to be "inviscid"  
(i.e., non-viscous) 非黏性流體

$$\text{Mathematically : } \mu = 0$$

→ **Question:** 為何要假設為理想流體？

**Answer:**

假設為理想流體即表示流體粒子間、或流體與邊界間無黏滯力作用，故所有加諸在流體上之力，均用以產生加速度，無需克服阻力，亦無能量損失。

1

## 2. 1-D Euler's Eqn. (along the streamline)



Euler (Swiss, 1707-1783)

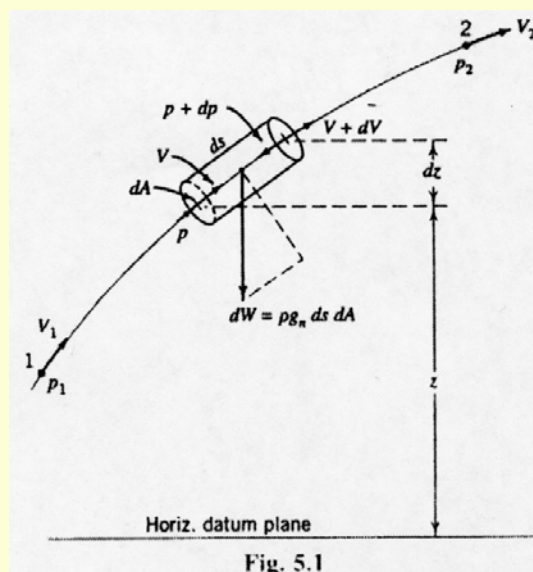


Fig. 5.1

2

因為是 Inviscid fluid ( $\mu = 0$ )  $\rightarrow$  No viscous force (無需考慮黏滯剪應力  $\tau$ )

$\rightarrow$  所受到的力：① Pressure, ② Gravity

① Pressure force :

$$P \cdot dA - (P + dP)dA = -dP \cdot dA$$

② Gravity force :

$$dW = \rho g \cdot dA \cdot ds$$

$$\begin{aligned} \text{Streamline dir. : } -dW \cdot \sin \theta &= -\rho g \cdot dA \cdot ds \cdot \frac{dz}{ds} \\ &= -\rho g \cdot dA \cdot dz \end{aligned}$$

3

③  $F_s = m \cdot a_s$

$$F_s = (-dP \cdot dA - \rho g \cdot dA \cdot dz)$$

$$m = \rho \cdot dA \cdot ds$$

$$a_s = V \cdot \frac{dV}{ds} \quad (\text{Recall Chap.3})$$

$$-dP \cdot dA - \rho g \cdot dA \cdot dz = (\rho \cdot dA \cdot ds) \left( V \cdot \frac{dV}{ds} \right)$$

$$-dP - \rho g \cdot dz = \rho V \cdot dV$$

$$\rightarrow \frac{dP}{\rho} + g \cdot dz + V \cdot dV = 0$$

$$\text{or } \boxed{\frac{dP}{\rho g} + dz + \frac{dV^2}{2g} = 0} \quad \text{1-D Euler's eqn. (along the streamline)}$$

For **incompressible fluid**: ( $\rho = \text{const.}$ )

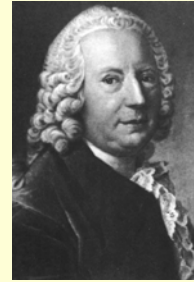
$$d \left( \frac{P}{\rho g} + z + \frac{V^2}{2g} \right) = 0$$

4

### 3. Bernoulli's Eqn. along the Streamline

Integrating 1-D Euler's eqn. (along the streamline)

$$\frac{P}{\gamma} + z + \frac{V^2}{2g} = \text{constant} = H$$



Bernoulli (Swiss, 1700-1782)

**Bernoulli's eqn. (along the streamline)**

- ◎ **Assumptions (適用條件)** :
- ①  $\mu = 0$  (Inviscid fluid) 理想流體
  - ②  $\rho = \text{const.}$  (Incompressible fluid)
  - ③ Along the streamline (1-D)
  - ④ steady flow

5

**Bernoulli's eqn. is a useful relationship between  $P$ ,  $V$ , and  $z$**

where  $H \equiv$  Total head (總水頭)

$\frac{P}{\gamma} \equiv$  pressure head (壓力水頭)

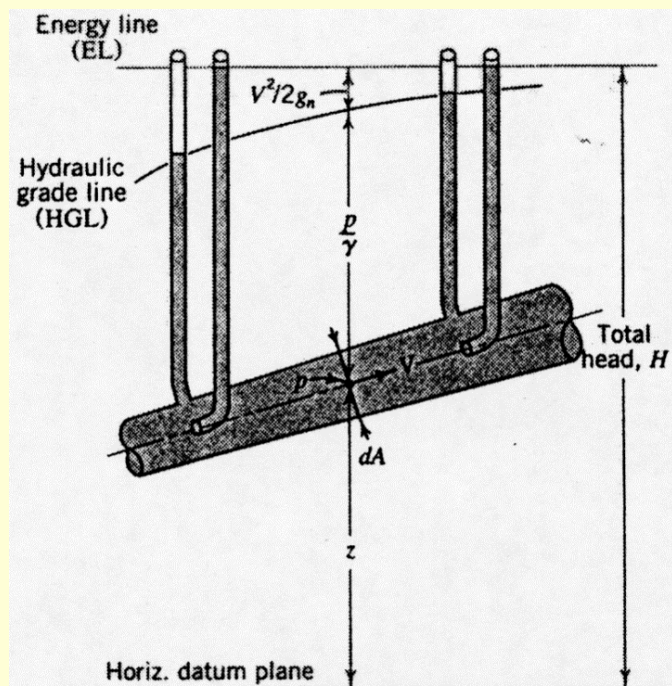
$z \equiv$  elevation head (高度水頭)

$\frac{V^2}{2g} \equiv$  velocity head (速度水頭)



6

#### 4. Energy Line (EL, 能量線) and Hydraulic Grade Line (HGL, 水力坡降線)



7

① Energy line (EL)  $\equiv$  Total head line (可用Stagnation Tube量測)

$$\left( \frac{P}{\gamma} + z + \frac{V^2}{2g} \right) \text{ 總和之連線}$$

② Hydraulic grade line (HGL)  $\equiv$  Piezometric head line  
(可用Piezometer量測)

$$\left( \frac{P}{\gamma} + z \right) \text{ 總和之連線 (稱為piezometric head or hydraulic head)}$$

8

## Applications of Bernoulli's Equation (BE)

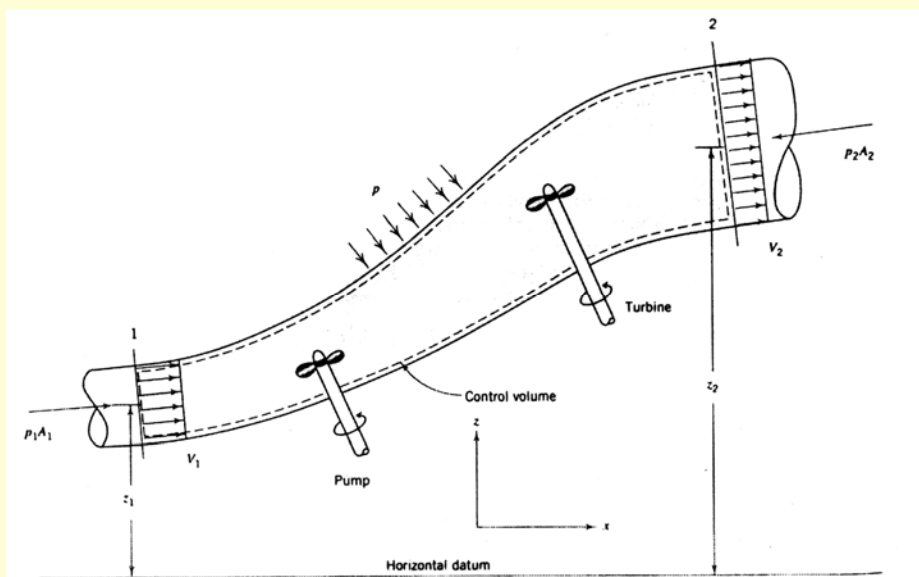
Type 1: Manometer (壓力計)  
BE

Type 2: Manometer (壓力計)  
CE  
BE

Type 3: CE  
BE

9

## 5. Work-Energy Equation (功-能方程式)



10

● **Mechanical work-energy principle:**

(Heat transfer and internal energy are neglected.)

$$dW = dE$$

where  $dW$  = the work done on a fluid system

$dE$  = the change in P.E. and K.E. of a fluid system

$$\rightarrow \frac{dW}{dt} = \frac{dE}{dt}$$

① For steady flow and incompressible fluid:

$$\frac{dE}{dt} = \iiint_{c.s.} e \rho \bar{V} \cdot d\bar{A}$$

$$\text{where } e = \frac{E}{m} = \frac{\frac{1}{2}mV^2 + mgz}{m} = \frac{V^2}{2} + gz$$

11

$$\begin{aligned} \frac{dE}{dt} &= \iiint_{c.s.} \rho \left( \frac{V^2}{2} + gz \right) \bar{V} \cdot d\bar{A} \\ &= \rho \left( \frac{V_2^2}{2} + gz_2 \right) V_2 A_2 - \rho \left( \frac{V_1^2}{2} + gz_1 \right) V_1 A_1 \\ &= Q\gamma \left[ \left( \frac{V_2^2}{2g} + z_2 \right) - \left( \frac{V_1^2}{2g} + z_1 \right) \right] \end{aligned}$$

②  $\frac{dW}{dt}$  : Two parts

(1) Surface forces: <i> Normal: pressure (✓)

<ii> Shear: friction (✗)

$$\begin{aligned} \frac{dW}{dt} &= \iiint_{c.s.} (-pd\bar{A}) \cdot \bar{V} \quad (\text{Power} = \bar{F} \cdot \bar{V}) \\ &= P_1 A_1 V_1 - P_2 A_2 V_2 \\ &= Q(P_1 - P_2) \end{aligned}$$

12

$$(2) \text{ Mechine work: Turbine } \frac{dW}{dt} = -Q\gamma E_T$$

$$\text{Pump } \frac{dW}{dt} = +Q\gamma E_P$$

where  $E_T$  = energy extracted by turbine per unit weight of fluid  
 $E_P$  = energy added by pump per unit weight of fluid

$$\Rightarrow \frac{dW}{dt} = \frac{dE}{dt}$$

$$= Q(P_1 - P_2) + (Q\gamma E_P - Q\gamma E_T)$$

$$= Q\gamma \left( \frac{P_1}{\gamma} - \frac{P_2}{\gamma} \right) + Q\gamma (E_P - E_T)$$

$$= Q\gamma \left( \frac{P_1}{\gamma} - \frac{P_2}{\gamma} + E_P - E_T \right)$$

$$= Q\gamma \left[ \left( \frac{V_2^2}{2g} + z_2 \right) - \left( \frac{V_1^2}{2g} + z_1 \right) \right]$$

13

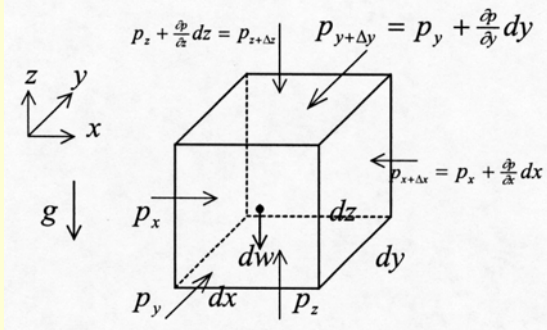
$$\therefore \boxed{\frac{P_1}{\gamma} + z_1 + \frac{V_1^2}{2g} + E_P = \frac{P_2}{\gamma} + z_2 + \frac{V_2^2}{2g} + E_T} \quad \text{Work-Energy Equation}$$

Power:  $\frac{Q\gamma (E_T \text{ or } E_P) \frac{J}{s}}{1000} = kW \quad (\text{kilo watt})$

14



## 6. 3-D Euler's Equation in Flowfield



Without viscosity (No shear force)

→ Only Pressure (normal stress) and gravity (body force)

$$\textcircled{1} \quad \sum F_x = P_x dy dz - \left( P_x + \frac{\partial P}{\partial x} dx \right) dy dz = -\frac{\partial P}{\partial x} dx dy dz$$

$$\textcircled{2} \quad \sum F_y = P_y dx dz - \left( P_y + \frac{\partial P}{\partial y} dy \right) dx dz = -\frac{\partial P}{\partial y} dx dy dz$$

$$\textcircled{3} \quad \sum F_z = P_z dx dy - \left( P_z + \frac{\partial P}{\partial z} dz \right) dx dy - \rho dx dy dz \cdot g$$

$$= -\frac{\partial P}{\partial z} dx dy dz - \rho g dx dy dz$$

15

We know :  $a_x = u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} + \frac{\partial u}{\partial t} = \frac{Du}{Dt}$

$$a_y = u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} + \frac{\partial v}{\partial t} = \frac{Dv}{Dt}$$

$$a_z = u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} + \frac{\partial w}{\partial t} = \frac{Dw}{Dt}$$

$$\vec{F} = m\vec{a} = (\rho dx dy dz)\vec{a}$$

$$\textcircled{1} \quad F_x = ma_x = (\rho dx dy dz)a_x = -\frac{\partial P}{\partial x} dx dy dz$$

$$\therefore \rho a_x = \rho \left[ u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} + \frac{\partial u}{\partial t} \right] = -\frac{\partial P}{\partial x}$$

16

$$\textcircled{2} F_y = ma_y = (\rho dx dy dz) a_y = -\frac{\partial P}{\partial y} dx dy dz$$

$$\therefore \rho a_y = \rho \left[ u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} + \frac{\partial v}{\partial t} \right] = -\frac{\partial P}{\partial y}$$

$$\textcircled{3} F_z = ma_z = (\rho dx dy dz) a_z = -\frac{\partial P}{\partial z} dx dy dz - \rho g dx dy dz$$

$$\therefore \rho a_z = -\frac{\partial P}{\partial z} - \rho g = \rho \left[ u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} + \frac{\partial w}{\partial t} \right]$$

整理如下： $\rho a_x = \rho \frac{Du}{Dt} = -\frac{\partial P}{\partial x} + \rho g_x$

$$\rho a_y = \rho \frac{Dv}{Dt} = -\frac{\partial P}{\partial y} + \rho g_y$$

$$\rho a_z = \rho \frac{Dw}{Dt} = -\frac{\partial P}{\partial z} + \rho g_z = -\frac{\partial P}{\partial z} - \rho g$$

17

令  $\bar{g} = g_x \hat{i} + g_y \hat{j} + g_z \hat{k}$       則  $g_x = g_y = 0, g_z = -g$

故 Euler's Eqn. 通式  $\rho \frac{D\bar{V}}{Dt} = -\nabla P + \rho \bar{g}$

⇒ It can be solved!      **4 unknowns** :  $u, v, w, P$

by      **3 eqns. of motion** ( $x, y, z$  方向)

and      **1 continuity eqn.**  $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$

**3-D Euler's Eqn. is an equation of motion for ideal and incompressible fluid.**

**In Chapter 9, we will talk about the equation of motion for real fluids, which is Navier-Stokes Equation.**

18

## 7. Bernoulli's Eqn. in Flowfield

Integrating 3-D Euler's eqn. for incompressible fluid and steady flow

$$\times dx \quad \textcircled{1} \quad -\frac{1}{\rho} \frac{\partial p}{\partial x} = u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z}$$

$$\times dy \quad \textcircled{2} \quad -\frac{1}{\rho} \frac{\partial p}{\partial y} = u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z}$$

$$\times dz \quad \textcircled{3} \quad -\frac{1}{\rho} \frac{\partial p}{\partial z} - g = u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z}$$

---


$$\begin{aligned} \sum &\Rightarrow -\frac{1}{\rho} \left( \frac{\partial P}{\partial x} dx + \frac{\partial P}{\partial y} dy + \frac{\partial P}{\partial z} dz \right) \\ &= \left( u \frac{\partial u}{\partial x} dx + v \frac{\partial u}{\partial y} dx + w \frac{\partial u}{\partial z} dx \right) + \left( u \frac{\partial v}{\partial x} dy + v \frac{\partial v}{\partial y} dy + w \frac{\partial v}{\partial z} dy \right) \\ &\quad + \left( u \frac{\partial w}{\partial x} dz + v \frac{\partial w}{\partial y} dz + w \frac{\partial w}{\partial z} dz \right) + g dz \end{aligned}$$

19

$$\begin{aligned} \Rightarrow -\frac{1}{\rho} (dP) &= \left[ \frac{\partial \left( \frac{u^2}{2} \right)}{\partial x} dx + \frac{\partial \left( \frac{v^2}{2} \right)}{\partial x} dx + \frac{\partial \left( \frac{w^2}{2} \right)}{\partial x} dx \right] \\ &\quad + \left[ \frac{\partial \left( \frac{u^2}{2} \right)}{\partial y} dy + \frac{\partial \left( \frac{v^2}{2} \right)}{\partial y} dy + \frac{\partial \left( \frac{w^2}{2} \right)}{\partial y} dy \right] \\ &\quad + \left[ \frac{\partial \left( \frac{u^2}{2} \right)}{\partial z} dz + \frac{\partial \left( \frac{v^2}{2} \right)}{\partial z} dz + \frac{\partial \left( \frac{w^2}{2} \right)}{\partial z} dz \right] \end{aligned}$$

20

$$\begin{aligned}
& \left[ -v \frac{\partial v}{\partial x} dx - w \frac{\partial w}{\partial x} dx - u \frac{\partial u}{\partial y} dy - w \frac{\partial w}{\partial y} dy - u \frac{\partial u}{\partial z} dz - v \frac{\partial v}{\partial z} dz \right] \\
& + \left( v \frac{\partial u}{\partial y} dx + u \frac{\partial v}{\partial x} dy \right) + \left( w \frac{\partial u}{\partial z} dx + u \frac{\partial w}{\partial x} dz \right) + \left( w \frac{\partial v}{\partial z} dy + v \frac{\partial w}{\partial y} dz \right) + g dz \\
& = d \left( \frac{u^2}{2} + \frac{v^2}{2} + \frac{w^2}{2} \right) + \left[ \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) (u dy - v dx) \right] + \left[ \left( \frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right) (v dz - w dy) \right] \\
& + \left[ \left( \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right) (w dx - u dz) \right] + g dz
\end{aligned}$$

$$\begin{aligned}
\left( \times \frac{1}{g} \right) \Rightarrow -\frac{dP}{\gamma} &= \frac{d(u^2 + v^2 + w^2)}{2g} \\
&+ \frac{1}{g} \left[ \Omega_x (v dz - w dy) + \Omega_y (w dx - u dz) + \Omega_z (u dy - v dx) \right] + dz
\end{aligned}$$

21

⇒ Integration :

$$\frac{P}{\gamma} + \frac{V^2}{2g} + z = H - \frac{1}{g} \int \left[ \Omega_x (v dz - w dy) + \Omega_y (w dx - u dz) + \Omega_z (u dy - v dx) \right]$$

● Bernoulli's eqn. (any two points in flowfield) valid for ①  $\mu = 0$  (Euler's eqn.)

②  $\rho = \text{const}$

③ steady flow

④ irrotational ( $\bar{\Omega} = 0$ )

● If rotational, only valid when  $(v dz - w dy) = (w dx - u dz) = (u dy - v dx) = 0$

$$\Rightarrow \frac{dx}{u} = \frac{dy}{v} = \frac{dz}{w} \quad (\text{streamline equation})$$

⇒ Bernoulli's eqn. only valid along streamline in rotational flows.

22